

**PREPARED FOR:**



Neuvokas Corp.

13206 #6 Rd, PO BOX 220

Ahmeek, MI 49901

(906) 934-2661

**DESIGN COMPUTATIONS FOR:**

1,500 Gallon Capacity Tank

(Septic or Grease Trap)

AASHTO H-10 Loading

**SPECIALTY ENGINEERING SERVICES PROVIDED BY:**

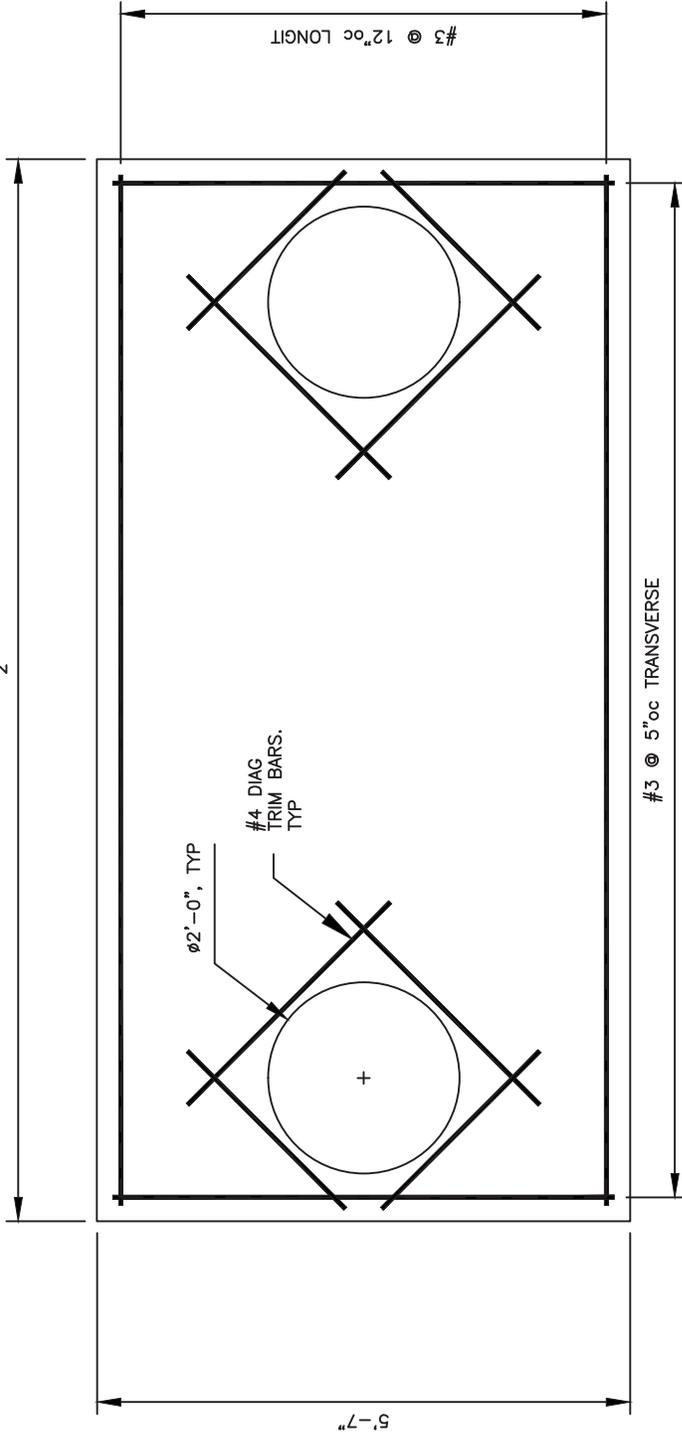
**Concrete Engineering Solutions, LLC**

101 Pineview Estates  
Mountain Top, PA 18707  
Phone: 570-868-2081  
Fax: 570-868-2082



3/11/16

11'-1 1/2"



(NOTE: REINF. MAY BE REDUCED BY 50% IN OUTER 1/4 ENDS OF SLAB)

TOP SLAB PLAN

(2)ADD'L #3 TYP



TOP SLAB SECTION

- NOTES:
- DESIGN IS IN ACCORDANCE WITH ASTM C1227, ACI440 AND C890
  - LIVE LOAD = A-8 (ASHTO H-10)
  - EARTH FILL FOR DESIGN = 1' - 2'
  - WATER TABLE ASSUMED AT 6' BELOW GRADE
  - CONCRETE STRENGTH = 5000psi
  - REINFORCING: NEUVOKAS GATORBAR PER ASTM 7205 (F<sub>u</sub>=145KSI)
  - PIPE OPENINGS, SIZE AND LOCATION, AS REQUIRED
    1. PROVIDE ADDITIONAL REINFORCING AROUND OPENINGS >12" EQUAL TO THE BARS INTERRUPTED BY THE OPENING, 1/4 EACH SIDE AND IN THE SAME PLANE
    2. ADD (2)#3 DIAGONAL TRIM BARS AT OPENINGS
  - LIFTING AND HANDLING SHALL CONFORM TO OSHA STANDARDS

PREPARED FOR:



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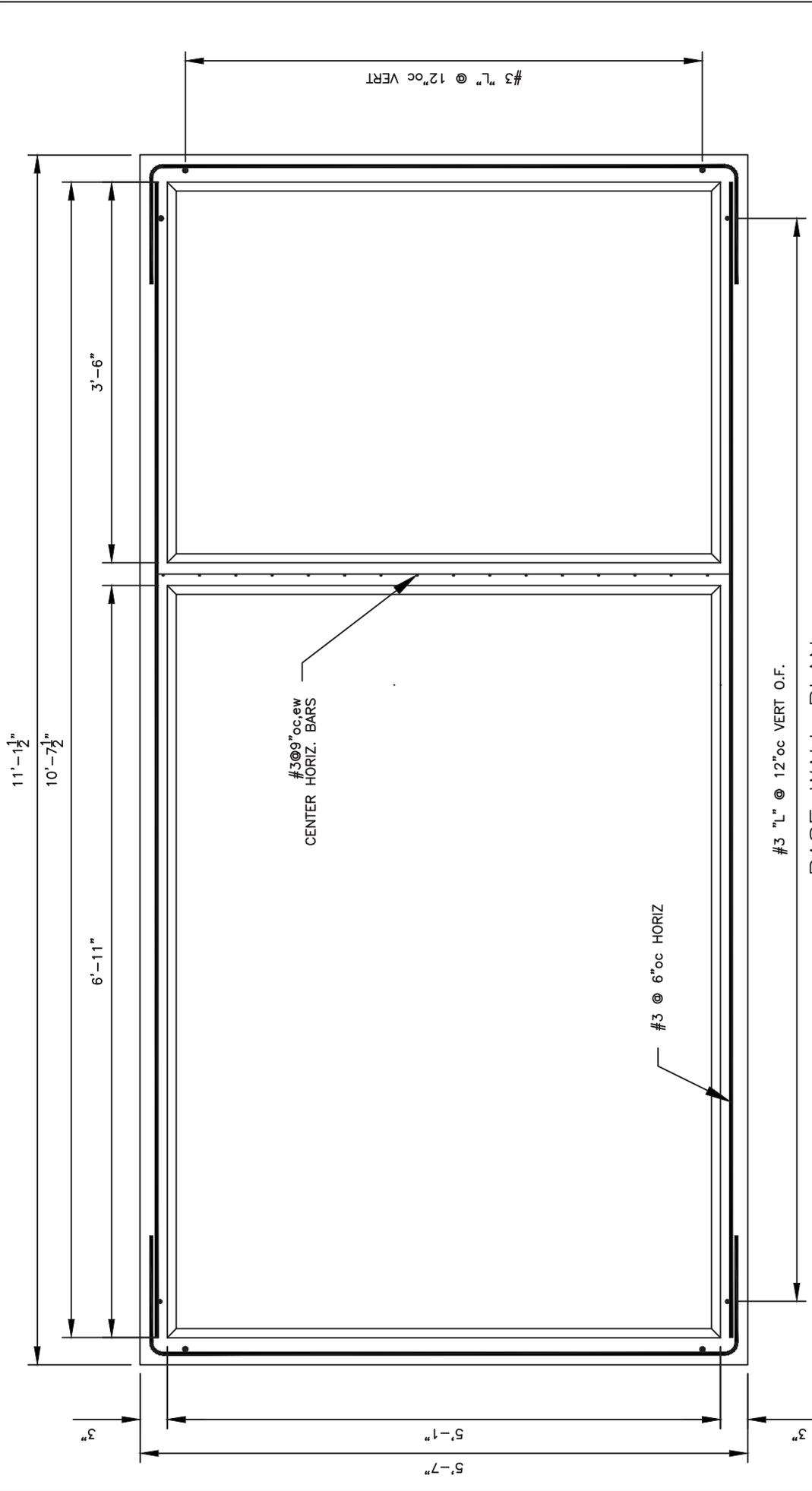


REV. NO.	DATE	REVISION

SHEET TITLE: SUMMARY  
DETAIL

PROJECT: 1,500 GALLON 2-COMPARTMENT  
SEPTIC TANK

SCALE: N.T.S.	DATE: 3/11/16	DRAWN BY: SDG	DWG. I.D.:	S-01
CES PROJ. NO.:	16-95.01		SHT. NO.:	1 OF 3



BASE WALL PLAN

REV. NO.	DATE	REVISION
SHEET TITLE: SUMMARY DETAIL		
PROJECT: 1,500 GALLON 2-COMPARTMENT SEPTIC TANK		
SCALE: N.T.S.	DATE: 3/11/16	DWG. I.D. S-02
CES PROJ. NO.: 16-95.01	DRAWN BY: SDG	SHT. NO. 2 OF 3

PREPARED FOR:



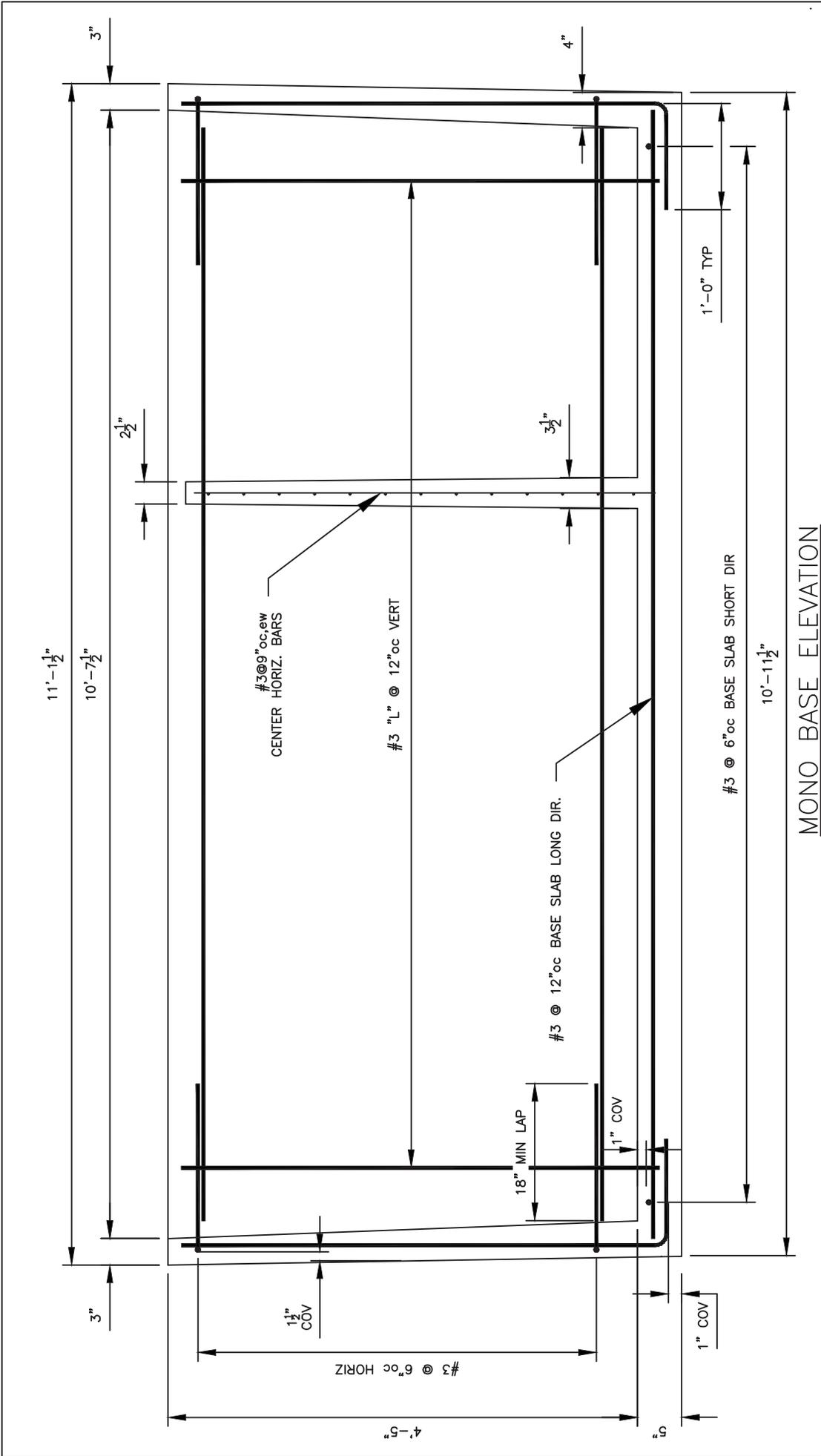
13206 #6 Rd, PO BOX 220  
AHMEEK, MI 49901  
(906) 934-2661

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  - 7.2. ADD (2)#3 DIAGONAL TRIM BARS AT OPENINGS
  - LIFTING AND HANDLING SHALL CONFORM TO OSHA STANDARDS



MONO BASE ELEVATION

REV. NO.	DATE	REVISION
SHEET TITLE: SUMMARY DETAIL		
PROJECT: 1,500 GALLON 2-COMPARTMENT SEPTIC TANK		
SCALE: N.T.S.	DATE: 3/11/16	DWG. I.D. S-03
CES PROJ. NO.: 16-95.01	DRAWN BY: SDG	SHT. NO. 3 OF 3

PREPARED FOR:



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# CONCRETE ENGINEERING SOLUTIONS, LLC

101 PINEVIEW ESTATES  
MOUNTAIN TOP, PA 18707  
PHONE: 570-868-2081  
FAX: 570-868-2082

Client: <u>Neuvokas</u>	Description: Tank Design 2-Compartment
Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By: <u>SDG</u> Date: <u>3/11/2016</u>	Basalt Fiber Reinforced Polymer

**Maximum Inside Dimensions**

Length	10.46 ft
Width	4.58 ft
Height	4.42 ft

**Member Thickness**

Top Slab	8.00 in
Walls	3.50 in
Base Slab	5.00 in

**Base Extension**    0.00 in LS    0.00 in SS

AASHTO      ASTM  
HS 10      A- 8

**Design Live Load**

Wheel Load	8 kips
Impact	1.3

**Earth Fill For Design**

2.00 ft Max
1.00 ft Min

**Top of Cover Above Grade**

0.00 ft

Lateral Earth Pressure, ka =

0.333

EP(h)	40 pcf (dry)
	82 pcf (saturated)

Surcharge    40 psf

Max Depth    8.00 ft

Water Table Elevation    6.00 ft below grade

**Materials**

Concrete Strength, f'c =	5000 psi
Tensile Strength, fu* =	145000 psi
Allowable ffu = 0.7 fu* =	101500 psi
Concrete Density, Wc	150 pcf
Soil Density, Ws	120 pcf
Water Density, Ww	62.4 pcf

**Load Factors**

Live Load	1.6
Dead Load	1.2
Earth Load	1.6

Structure Watertight?    Yes

Minimum Floatation SF    1.1

**Structure Components:**

Mono Top Riser Height	0.00 ft
Riser #1 Height	4.42 ft
Riser #2 Height	0.00 ft
Riser #3 Height	0.00 ft
Mono Base Riser Height	0.00 ft
Total Inside Height	4.42 ft

Depth		Lateral Earth Pressure				Concrete	
t-o-w	b-o-w	Pe top	Pe bot	Surch	Avg	Vol	Wgt
(ft)	(ft)	(psf)	(psf)	(psf)	(psf)	(cy)	(Tons)
2.67	2.67	107	107	40	147	1.41	2.85
2.67	7.08	107	328	40	257	1.49	3.02
7.08	7.08	328	328	40	368	0.00	0.00
7.08	7.08	328	328	40	368	0.00	0.00
7.08	7.08	328	328	40	368	0.88	1.78
<b>Totals</b>						<b>3.78</b>	<b>7.65</b>

\*\* Openings not subtracted

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Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By <u>SDG</u> Date: <u>3/11/16</u>	References

- (1) AASHTO Standard Specifications for Highway Bridges, 17th Edition
- (2) ASTM C857 "Minimum Structural Design Loading for Underground Precast Concrete Utility Structures
- (3) ACI318 & ACI440
- (4) "Moments and Reactions for Rectangular Plates" Engineering Monograph 27, U.S. Bureau of Reclamation

[http://www.usbr.gov/pmts/hydraulics\\_lab/pubs/EM/EM27.pdf](http://www.usbr.gov/pmts/hydraulics_lab/pubs/EM/EM27.pdf)

$E_c = 57000 \cdot \sqrt{f'_c} = 4031 \text{ ksi} \quad (1) 8.7.1$

$E_f = 6000 \text{ ksi} \quad (1) 8.7.2$

$n = E_f / E_c = 1.49 \quad (1) 8.15.3.4$

$M_{cr} = f_r \cdot b \cdot T^2 / 6 \quad T = \text{Member Thickness} \quad (1) 8.13.3$

Member Design Width,  $b = 12 \text{ in}$

**Moment Equations**

Plate Fixed on 3 sides,  $M = W_{avg} \times H^2 \times C_m$

$C_m / C_v =$  Moment or Shear Coefficient from Ref (4)

interpolated to the nearest 0.1

L/H Ratio of 4 or greater considered a cantilever

Simple Span Moments =  $W \times S^2 / 8$  (Uniform)

$= P \times S / 4$  (Concentrated)

Fixed End Moments =  $W \times L^2 / 12$

$p = A_s / b d$

$k = \sqrt{(r n^2 \cdot 2m) - r n}$

$j = 1 - k / 3$

$F_s = M / (A_s \cdot j \cdot d)$

**Shear Equations**

Plate Fixed on 3 sides,  $V = W_{avg} \times H \times C_v$

Shear Capacity,  $V_n = 2 \sqrt{f'_c} \cdot b d \quad (1) 8.16.6.1$

Minimum Flexural Reinforcing

$\mu > 1.2 M_{cr} =$ ; Waived if  $A_s \text{ Prov} > 4/3 A_s \text{ Req}$

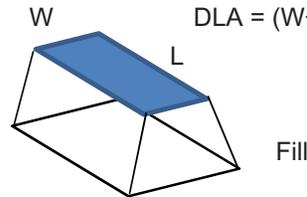
(1) 8.17.7.1.1 and 8.17.7.1.2

For Concentrated Wheel Load

Distribution Width,  $e = 4 + .06S \quad (1) 3.24.3$

For Wheel Load Distributed Through Fill (2) and (3)

$DLA = (W + 1.75 \text{ Fill}) \cdot (L + 1.75 \text{ Fill})$

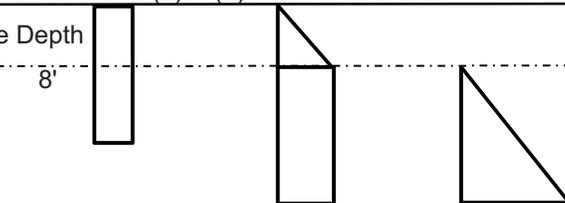


Lateral Soil Pressure - Ref (2) & (3)

Surcharge Depth  
8'

Finished Grade

Water Table Elevation



LL Surcharge

EP(h) Dry

EP(h) Saturated

0.5% Wheel Load

$K_a \cdot W_s \cdot H$

$(W_w + K_a \cdot (W_s - W_w)) \cdot H$

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Client: <u>Neuvokas</u>	Description: Tank Design 2-Compartment
Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By <u>SDG</u> Date: <u>3/11/16</u>	Top Slab Design - Concentrated Load, Min Fill

Span 4.87 ft Short Dir 10.75 ft Long Dir

Design As a 1-Way Slab? Yes Distribution Steel (As/S<sup>1.5</sup>) Used for Long Direction

Single Layer of Reinforcing? Yes

Dead Load	Live Load
Earth Fill <span style="margin-left: 100px;">120 psf</span>	Wheel Load, Pw = <span style="margin-left: 100px;">8 kips/ft</span>
Concrete <span style="margin-left: 100px;">100 psf</span>	Impact, I <span style="margin-left: 100px;">1.3</span>
Other <span style="margin-left: 100px;">psf</span>	Distribution Width, e <span style="margin-left: 100px;">4.292 ft</span>
Total <span style="margin-left: 100px;">220 psf</span>	Strip Load =P+I/e <span style="margin-left: 100px;">2.42 kips/ft</span>

Bar Cover 1.00 in

Moments	Short Dir. B.F.	Long Dir. B.F.
Portion Of Uniform Load	1.000	0.000
Dead Load Moment, Mdl	0.65 kip-ft	0.00 kip-ft
Portion Of Concentrated Loa	1.000 Short	0.000 Long
Live Load Moment, Mll	2.953 kip-ft	0.00 kip-ft
Mu =	5.508 kip-ft	0.00 kip-ft
Vu =	4.52 kips (DL*Span/2*DLF + P*LLF)	

\*See Following Sheet For Capacity & FRP Reinforcing.

**Client:** Neuvokas  
**Project Name:** Standard Tank Design  
**Structure Name:** 1,500 Gallon Tank

## Member: Top Slab

Member Thickness:	8.0"
Bar Cover:	1.0"
Concrete Strength, f <sub>c</sub> :	5000 PSI
Beam Width, b:	12.0"

<b>Factored Moment, Mu:</b>	<b>5.93 K-FT</b>
<b>Service Moment, Ms:</b>	<b>3.60 K-FT</b>

### Calculate Flexural Capacity:

Bar Size/Spacing: #3 @ 5.0" o.c. (A<sub>f</sub> Provided =0.27 sq.in./ft.)

$$M_n = A_f \cdot f_{fu} \cdot (d - \beta_1 \cdot c_b / 2) = 14.35 \text{ k-ft}$$

$$c_b = \epsilon_{cu} / (\epsilon_{cu} + \epsilon_{fu}) \cdot d = 1.03"$$

Where,  $\beta_1 = [0.85 - 0.05 \cdot (f_c - 4 \text{ ksi})] = 0.80$

$$d = \text{Thickness} - \text{Cover} - 1/2 \text{ Bar Dia.} = 6.81"$$

### Check Min A<sub>s</sub> Provided:

Minimum Reinforcement,  $\rho_f, \rho_s = 0.0015 \leq 0.0051 \leq 0.0036$   
 Note, If Middle Value > 0.0036, Use 0.0036.  
 A<sub>f,min</sub> = 0.35 Sq.in./ft. **NG**, **4/3 A<sub>s</sub> Provided, OK**

### Check Max Bar Spacing & Serviceability:

$\rho_f = A_f / b \cdot d = 0.00324$       E<sub>f</sub> = 6000 psi  
 $\rho_{fb} = \beta_1 \cdot f_c / f_{tu} \cdot E_f \cdot \epsilon_{cu} / (E_f \cdot \epsilon_{cu} + f_{fu}) = 0.00490$       f<sub>fu</sub> = 101500 psi

Check if Tension-Controlled:  $\rho_f / \rho_{fb} = 0.661$  (If Greater than 1.0, compression-controlled)

$\phi M_n = 7.89 \text{ k-ft}$        $\phi = 0.55$  (0.55 if tension controlled,  
 Mu = 5.93 k-ft **OK**      0.65 if compression)

$$s_{max} = 1.15 E_f w / (f_{fs} \cdot k_b) - 2.5 c_c \leq 0.92 \cdot E_f w / (f_{fs} \cdot k_b)$$

8.21 < 8.94      kb=0.7  
 (Say OK) **OK**      w=0.028  
 nf=1.49  
 $k = \text{SQRT}(2 \rho_f \cdot n_f + (\rho_f \cdot n_f)^2) = 0.094$   
 $l_{cr} = b d^3 / 3 \cdot k^3 + n_f \cdot A_f \cdot d^2 = 16.083$   
 cc = 1.188  
 $f_{fs} = M_s \cdot n_f \cdot d (1 - k) / l_{cf} = 24.69 \text{ ksi}$

**Check Creep Rupture:**      f<sub>fs</sub> Max = 0.5 f<sub>fu</sub> = 50.75 ksi **OK**  
 (Under Sustained Loading)

### Check Shear:

**Factored Shear, Vu:** 4.52 KIPS  
**Shear Capacity,  $\phi V_n$ :** 5.43 KIPS **OK** (Based Upon Unreinforced Concrete)  
 ( $\phi V_n = 0.6 (4/3 \cdot \sqrt{f_c} \cdot b \cdot h / 1000)$ )

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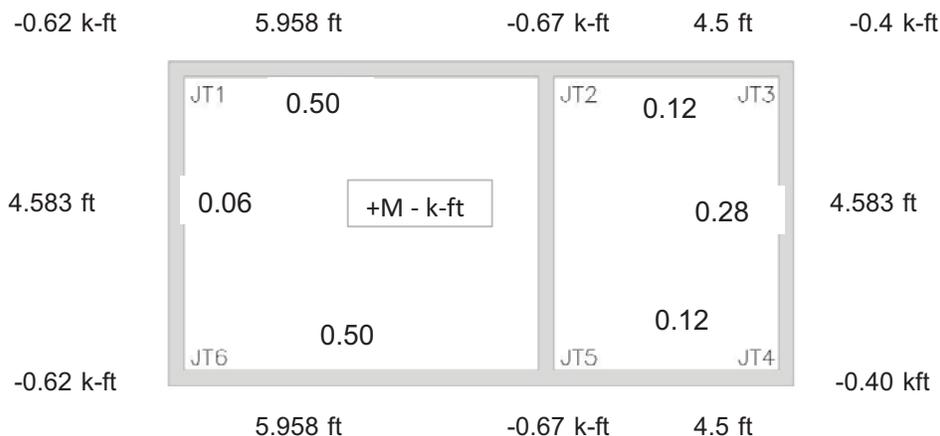
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Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By: <u>SDG</u> Date: <u>3/11/16</u>	

Uniform Load, w = 0.257 ksf

Carry over 0.5

Joint	1	2	2	3	3	4	4	5	5	6	6	1
Thickness	3.50	in		3.50	in		3.50	in		3.50	in	
Seg Length	5.96	ft		4.50	ft		4.58	ft		4.5	ft	
Dist Factor	0.435	0.430	0.570	0.505	0.495	0.495	0.505	0.570	0.430	0.435	0.565	0.565
FEM	0.76	-0.76	0.43	-0.43	0.45	-0.45	0.43	-0.43	0.76	-0.76	0.45	-0.45
1st Dist	-0.14	0.14	0.19	-0.01	-0.01	0.01	0.01	-0.19	-0.14	0.14	0.18	-0.18
Carryover	0.07	-0.07	0.00	0.09	0.00	0.00	-0.09	0.00	0.07	-0.07	-0.09	0.09
2nd Dist	-0.07	0.03	0.04	-0.05	-0.05	0.05	0.05	-0.04	-0.03	0.07	0.09	-0.09
Carryover	0.02	-0.03	-0.02	0.02	0.02	-0.02	-0.02	0.02	0.03	-0.02	-0.04	0.04
3rd Dist	-0.03	0.03	0.03	-0.02	-0.02	0.02	0.02	-0.03	-0.03	0.03	0.03	-0.03
Carryover	0.01	-0.01	-0.01	0.02	0.01	-0.01	-0.02	0.01	0.01	-0.01	-0.02	0.02
4th Dist	-0.01	0.01	0.01	-0.01	-0.01	0.01	0.01	-0.01	-0.01	0.01	0.02	-0.02
Carryover	0.01	-0.01	-0.01	0.01	0.01	-0.01	-0.01	0.01	0.01	-0.01	-0.01	0.01
5th Dist	-0.01	0.01	0.01	-0.01	-0.01	0.01	0.01	-0.01	-0.01	0.01	0.01	-0.01
Carryover	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
6th Dist	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Sum	0.62	-0.67	0.67	-0.40	0.40	-0.40	0.40	-0.67	0.67	-0.62	0.62	-0.62
+M =	0.50 k-ft		0.12 k-ft		0.28 k-ft		0.12 k-ft		0.50 k-ft		0.06 k-ft	
Reactions (k)	0.76	0.78	0.64	0.52	0.59	0.59	0.52	0.64	0.78	0.76	0.59	0.59



\*See Following Sheet For Capacity & FRP Reinforcing.

**Client:** Neuvokas  
**Project Name:** Standard Tank Design  
**Structure Name:** 1,500 Gallon Tank

## Member: Walls (Outside Face)

Member Thickness: 3.5"  
 Bar Cover: 1.5"  
 Concrete Strength, f<sub>c</sub>: 5000 PSI  
 Beam Width, b: 12.0"

**Factored Moment, Mu:** 1.07 K-FT  
**Service Moment, Ms:** 0.67 K-FT

### Calculate Flexural Capacity:

Bar Size/Spacing: #3 @ 6.0" o.c. (A<sub>f</sub> Provided =0.22 sq.in./ft.)

M<sub>n</sub>=A<sub>f</sub>\*f<sub>fu</sub>(d-β<sub>1</sub>\*c<sub>b</sub>/2): **1.71 k-ft**      c<sub>b</sub>=ε<sub>cu</sub>/(ε<sub>cu</sub>+ε<sub>fu</sub>)\*d= 0.44"  
 Where, β<sub>1</sub>=[0.85-.05\*(f<sub>c</sub>-4ksi)]= 0.80  
 d=Thickness-Cover-1/2Bar Dia.= 1.81"

### Check Min A<sub>s</sub> Provided:

Minimum Reinforcement, ρ<sub>f,ts</sub> =0.0015 ≤ 0.0092 ≤ 0.0036  
 Note, If Middle Value > 0.0036, Use 0.0036.  
 A<sub>f,min</sub>= 0.15 Sq.in./ft. **OK**

### Check Max Bar Spacing & Serviceability:

ρ<sub>f</sub> = A<sub>f</sub> / b \* d = 0.01016      E<sub>f</sub>= 6000 psi  
 ρ<sub>fb</sub>=β<sub>1</sub>\*f<sub>c</sub>/f<sub>tu</sub>\*E<sub>f</sub>\*ε<sub>cu</sub>/(E<sub>f</sub>\*ε<sub>cu</sub>+f<sub>fu</sub>) = 0.00875      f<sub>fu</sub>(Bends)= 56840 psi  
 (0.56\*f<sub>fu</sub>)  
 Check if Tension-Controlled: ρ<sub>f</sub>/ρ<sub>fb</sub> = 1.160 (If Greater than 1.0, compression-controlled)  
 φM<sub>n</sub>= **1.11 k-ft**      φ= 0.65 (0.55 if tension controlled,  
 Mu= **1.07 k-ft** **OK**      0.65 if compression)

s<sub>max</sub>=1.15E<sub>f</sub>w/(f<sub>fs</sub>\*k<sub>b</sub>)-2.5c<sub>c</sub> ≤ 0.92\*E<sub>f</sub>\*w/(f<sub>fs</sub>\*k<sub>b</sub>)      k<sub>b</sub>=0.7  
**8.79** < **10.41**      w=0.028  
**OK**      n<sub>f</sub>=1.49  
 k=SQRT(2ρ<sub>f</sub>\*n<sub>f</sub>+(ρ<sub>f</sub>\*n<sub>f</sub>)<sup>2</sup>)- 0.159  
 l<sub>cr</sub>=bd<sup>3</sup>/3\*k<sup>3</sup>+n<sub>f</sub>\*A<sub>f</sub>\*d<sup>2</sup>( 0.860  
 c<sub>c</sub>= 1.688  
 f<sub>fs</sub>=M<sub>s</sub>\*n<sub>f</sub>\*d(1-k)/l<sub>cf</sub>= 21.21 ksi

**Check Creep Rupture:**      f<sub>fs</sub> Max = 0.5f<sub>fu</sub>= 28.42 ksi **OK**  
 (Under Sustained Loading)

### Check Shear:

**Factored Shear, Vu:** **1.23 KIPS** =0.257KSF\*5.96'/2\*1.6LF  
**Shear Capacity, φV<sub>n</sub>:** **2.38 KIPS** **OK** (Based Upon Unreinforced Concrete)  
 (φV<sub>n</sub>=0.6(4/3\*√f<sub>c</sub>\*b\*h/1000)

**Client:** Neuvokas  
**Project Name:** Standard Tank Design  
**Structure Name:** 1,500 Gallon Tank

## Member: Walls (Inside Face)

Member Thickness:	3.5"
Bar Cover:	1.6"
Concrete Strength, f <sub>c</sub> :	5000 PSI
Beam Width, b:	12.0"

<b>Factored Moment, Mu:</b>	<b>0.80 K-FT</b>
<b>Service Moment, Ms:</b>	<b>0.50 K-FT</b>

### Calculate Flexural Capacity:

Bar Size/Spacing: #3 @ 6.0" o.c. (Af Provided =0.22 sq.in./ft.)

Mn=Af\*ffu(d-β1\*cb/2): **3.01 k-ft**      cb=εcu/(εcu+εfu)\*d= 0.26"  
 Where, β1=[0.85-.05\*(f<sub>c</sub>-4ksi)]= 0.80  
 d=Thickness-Cover-1/2Bar Dia.= 1.71"

### Check Min A<sub>s</sub> Provided:

Minimum Reinforcement, ρ<sub>f,ts</sub> =0.0015 ≤ 0.0051 ≤ 0.0036  
 Note, If Middle Value > 0.0036, Use 0.0036.  
 Af,min= 0.15 Sq.in./ft. **OK**

### Check Max Bar Spacing & Serviceability:

ρ<sub>f</sub> = Af / b \* d = 0.01075      Ef= 6000 psi  
 ρ<sub>fb</sub>=β1\*f<sub>c</sub>/ftu\*Ef\*εcu/(Ef\*εcu+ffu) = 0.00490      ffu= 101500 psi  
 Check if Tension-Controlled: ρ<sub>f</sub>/ρ<sub>fb</sub> = 2.193 (If Greater than 1.0, compression-controlled)  
 φMn= **1.95 k-ft**      φ= 0.65 (0.55 if tension controlled,  
 Mu= **0.80 k-ft** **OK**      0.65 if compression)

smax=1.15E<sub>f</sub>w/(f<sub>fs</sub>\*k<sub>b</sub>)-2.5c<sub>c</sub> ≤ 0.92\*Ef\*w/(f<sub>fs</sub>\*k<sub>b</sub>)      kb=0.7  
**11.98** < **13.16**      w=0.028  
**OK**      nf=1.49  
 k=SQRT(2ρ<sub>f</sub>\*nf+(ρ<sub>f</sub>\*nf)<sup>2</sup>)- 0.164  
 lcr=bd<sup>3</sup>/3\*k<sup>3</sup>+nf\*Af\*d<sup>2</sup>( 0.763  
 cc= 1.788  
 ffs=Ms\*nf\*d(1-k)/lcf= 16.78 ksi

**Check Creep Rupture:**      ffs Max = 0.5ffu= 50.75 ksi **OK**  
 (Under Sustained Loading)

# CONCRETE ENGINEERING SOLUTIONS, LLC

101 PINEVIEW ESTATES  
MOUNTAIN TOP, PA 18707  
PHONE: 570-868-2081  
FAX: 570-868-2082

Client: <u>Neuvokas</u>	Description: Tank Design 2-Compartment
Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By <u>SDG</u> Date: <u>3/11/16</u>	Base Slab Design

Span 4.87 ft Short Dir 10.75 ft Long Dir

Design As 1-Way?

Single Layer of Reinforcing?

**Dead Load**

**Live Load**

Earth Fill 240 psf

Wheel Load, Pw  kips/ft

Concrete 206 psf

Number Of Wheels

Other psf

Bearing Area 57 SF

Total 446 psf <-Controls

Uniform Live Load 280 ksf

Hydrostatic 94 psf

Bar Cover  in

Moments Short Dir. T.F. Long Dir. T.F.

Portion of Uniform Load 0.964 0.036

Dead Load Moment, Mdl 1.28 kip-ft 0.23 kip-ft

Live Load Moment, Mll 0.804 kip-ft 0.14 kip-ft

Mu = 2.82 kip-ft 0.51 kip-ft

Factored Shear, Vu 2.31 kips 0.19 kips

\*See Following Sheet For Capacity & FRP Reinforcing.

**Client:** Neuvokas  
**Project Name:** Standard Tank Design  
**Structure Name:** 1,500 Gallon Tank

## Member: Base Slab

Member Thickness:	5.0"
Bar Cover:	1.0"
Concrete Strength, f <sub>c</sub> :	5000 PSI
Beam Width, b:	12.0"

<b>Factored Moment, Mu:</b>	<b>2.82 K-FT</b>
<b>Service Moment, Ms:</b>	<b>2.08 K-FT</b>

### Calculate Flexural Capacity:

Bar Size/Spacing: #3 @ 6.0" o.c. (Af Provided =0.22 sq.in./ft.)

Mn=Af\*ffu(d-β1\*cb/2): 6.69 k-ft      cb=εcu/(εcu+εfu)\*d= 0.57"  
 Where, β1=[0.85-.05\*(f<sub>c</sub>-4ksi)]= 0.80  
 d=Thickness-Cover-1/2Bar Dia.= 3.81"

### Check Min A<sub>s</sub> Provided:

Minimum Reinforcement, ρ<sub>f,ts</sub> =0.0015 ≤ 0.0051 ≤ 0.0036  
 Note, If Middle Value > 0.0036, Use 0.0036.  
 Af,min= 0.22 Sq.in./ft. **OK**

### Check Max Bar Spacing & Serviceability:

ρ<sub>f</sub> = Af / b \* d = 0.00483      Ef= 6000 psi  
 ρ<sub>fb</sub>=β1\*f<sub>c</sub>/ftu\*Ef\*εcu/(Ef\*εcu+ffu) = 0.00490      ffu= 101500 psi

Check if Tension-Controlled: ρ<sub>f</sub>/ρ<sub>fb</sub> = 0.985 (If Greater than 1.0, compression-controlled)

φMn= 3.68 k-ft      φ= 0.55 (0.55 if tension controlled,  
 Mu= 2.82 k-ft **OK**      0.65 if compression)

smax=1.15E<sub>f</sub>w/(f<sub>fs</sub>\*k<sub>b</sub>)-2.5c<sub>c</sub> ≤ 0.92\*Ef\*w/(f<sub>fs</sub>\*k<sub>b</sub>)      kb=0.7  
 5.99 < 7.17      w=0.028  
 (Say OK) **NG**      nf=1.49  
 k=SQRT(2ρ<sub>f</sub>\*nf+(ρ<sub>f</sub>\*nf)<sup>2</sup>)- 0.113  
 lcr=bd<sup>3</sup>/3\*k<sup>3</sup>+nf\*Af\*d<sup>2</sup> 4.080  
 cc= 1.188  
 ffs=Ms\*nf\*d(1-k)/lcf= 30.80 ksi

**Check Creep Rupture:** ffs Max = 0.5ffu= 50.75 ksi **OK**  
 (Under Sustained Loading)

### Check Shear:

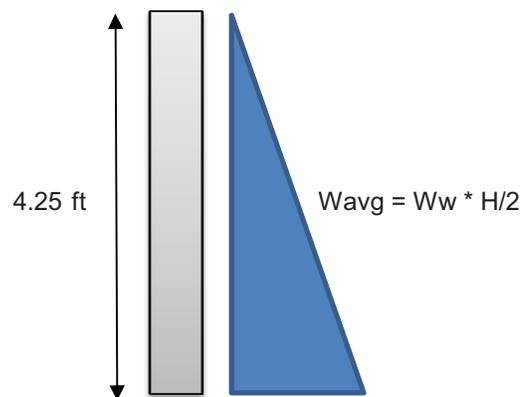
**Factored Shear, Vu:** 2.31 KIPS  
**Shear Capacity, φVn:** 3.39 KIPS **OK** (Based Upon Unreinforced Concrete)  
 (φVn=0.6(4/3\*√f<sub>c</sub>\*b\*h/1000))

# CONCRETE ENGINEERING SOLUTIONS, LLC

101 PINEVIEW ESTATES  
MOUNTAIN TOP, PA 18707  
PHONE: 570-868-2081  
FAX: 570-868-2082

Client: <u>Neuvokas</u>	Description: Tank Design 2-Compartment
Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By: <u>SDG</u> Date: <u>3/11/16</u>	Compartment Wall Design

Height, H	4.25 ft
Width	4.58 ft
Thickness	3 in
Avg Hyd. Pressure, Wavg	133 psf
Horiz Moment, M	0.35 kip-ft
Mu = M * 1.6	0.56 kip-ft
Horiz Shear, V	0.30 kips
Vu = V * 1.6	0.49 kips



\*See Following Sheet for Capacities and Reinforcing.

**Client:** Neuvokas  
**Project Name:** Standard Tank Design  
**Structure Name:** 1,500 Gallon Tank

## Member: Baffle

Member Thickness:	3.0"
Bar Cover:	1.4"
Concrete Strength, f <sub>c</sub> :	5000 PSI
Beam Width, b:	12.0"

<b>Factored Moment, Mu:</b>	<b>0.56 K-FT</b>
<b>Service Moment, Ms:</b>	<b>0.35 K-FT</b>

### Calculate Flexural Capacity:

Bar Size/Spacing: #3 @ 9.0" o.c. (Af Provided =0.15 sq.in./ft.)

Mn=Af\*ffu(d-β1\*cb/2): 1.68 k-ft      cb=εcu/(εcu+εfu)\*d= 0.22"  
 Where, β1=[0.85-.05\*(f<sub>c</sub>-4ksi)]= 0.80  
 d=Thickness-Cover-1/2Bar Dia.= 1.44"

### Check Min A<sub>s</sub> Provided:

Minimum Reinforcement, ρ<sub>f,ts</sub> =0.0015 ≤ 0.0051 ≤ 0.0036  
 Note, If Middle Value > 0.0036, Use 0.0036.  
 Af,min= 0.13 Sq.in./ft.      **OK**

### Check Max Bar Spacing & Serviceability:

ρ<sub>f</sub> = Af / b \* d = 0.00854      Ef= 6000 psi  
 ρ<sub>fb</sub>=β1\*f<sub>c</sub>/ftu\*Ef\*εcu/(Ef\*εcu+ffu) = 0.00490      ffu= 101500 psi  
 Check if Tension-Controlled: ρ<sub>f</sub>/ρ<sub>fb</sub> = 1.741 (If Greater than 1.0, compression-controlled)  
 φMn= 1.09 k-ft      φ= 0.65 (0.55 if tension controlled,  
 Mu= 0.56 k-ft      **OK**      0.65 if compression)

smax=1.15E<sub>f</sub>w/(f<sub>fs</sub>\*k<sub>b</sub>)-2.5c<sub>c</sub> ≤ 0.92\*Ef\*w/(f<sub>fs</sub>\*k<sub>b</sub>)      kb=0.7  
 9.32 < 10.58      w=0.028  
**OK**      nf=1.49  
 k=SQRT(2ρ<sub>f</sub>\*nf+(ρ<sub>f</sub>\*nf)<sup>2</sup>)- 0.147  
 lcr=bd<sup>3</sup>/3\*k<sup>3</sup>+nf\*Af\*d<sup>2</sup>( 0.367  
 cc= 1.563  
 ffs=Ms\*nf\*d(1-k)/lcf= 20.86 ksi

**Check Creep Rupture:**      ffs Max = 0.5ffu= 50.75 ksi      **OK**  
 (Under Sustained Loading)

### Check Shear:

**Factored Shear, Vu:** 0.49 KIPS  
**Shear Capacity, φVn:** 2.04 KIPS      **OK**      (Based Upon Unreinforced Concrete)  
 (φVn=0.6(4/3\*√f<sub>c</sub>\*b\*h/1000)

# CONCRETE ENGINEERING SOLUTIONS, LLC

101 PINEVIEW ESTATES  
MOUNTAIN TOP, PA 18707  
PHONE: 570-868-2081  
FAX: 570-868-2082

Client: <u>Neuvokas</u>	Description: Tank Design 2-Compartment
Project Name: <u>Standard Tank Design</u>	1,500 Gallon Tank
Calculated By <u>SDG</u> Date: <u>3/11/16</u>	Buoyancy Check

Bottom of Base Slab BFG	7.5 ft
Top of Cover Slab BFG	2.00 ft
Water Table BFG	6.00 ft
Structure Footprint (w/o Extension)	57.04 sf

**Downward Forces**

Earth Fill	13690 lbs
Concrete	15308 lbs
Soil Envelope	0.0 lbs
Holes	-2136 lbs
Compartment Wall	846 lbs
<b>Total</b>	<b>27707 lbs</b>

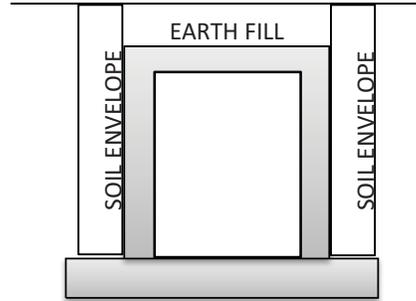
Upward Buoyant Force	5339 lbs
Difference	22368 lbs
Safety Factor	5.2 OK

Add Soil Wedge?

No

10

No Base Extension



**Subtract for Holes:**

	Qty		Vol (cf)	Wgt (lbs)
Top Slab				
24.in Diam	(2)		4.19	628.3
.in x .in	(0)		0.00	0
Fill			12.57	1508
Walls				
.in Diam	(4)		0.00	0
.in x .in	(0)		0.00	0
Base Slab				
.in Diam	(0)		0.00	0
.in x .in	(0)		0.00	0
<b>Total</b>			<b>16.76</b>	<b>2136</b>